Influence of the Electrolyte Concentration on the Smooth TiO$_2$ Anodic Coatings on Ti-6Al-4V

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Abstract: To obtain smooth TiO$_2$ coatings for building a new design of Ti-6Al-4V heart valve, the anodic oxidation technique in pre-spark conditions was evaluated. TiO$_2$ coating is necessary for its recognized biocompatibility and corrosion resistance. A required feature on surfaces in contact with blood is a low level of roughness ($R_a \leq 50$ nm) that does not favor the formation of blood clots. The present paper compares the coatings obtained by anodic oxidation of the Ti-6Al-4V alloy using H$_2$SO$_4$ at different concentrations (0.1–4 M) as electrolyte and applying different voltages (from 20 to 70 V). Color and morphological analysis of coatings are performed using optical and scanning microscopy. The crystalline phases were analyzed by glancing X-ray diffraction. By varying the applied voltage, different interference colors coatings were obtained. The differences in morphologies of the coatings caused by changes in acid concentration are more evident at high voltages, limiting the oxidation conditions for the desired application. Anatase phase was detected from 70 V for 1 M H$_2$SO$_4$. An increase in the concentration of H$_2$SO$_4$ decreases the voltage at which the transformation of amorphous to crystalline coatings occurs; i.e., with 4 M H$_2$SO$_4$, the anatase phase appears at 60 V.

Keywords: anodic oxidation; titanium dioxide; electrolyte concentration; sulfuric acid

1. Introduction

With the objective of building a new mechanical heart valve design [1], the Ti-6Al-4V alloy coated with titanium dioxide (TiO$_2$) has been selected as the building material [2]. TiO$_2$ coatings have demonstrated hemocompatibility properties appropriate for use in this type of prosthesis [3–5].

Ti-6Al-4V alloy (grade 5 in ASTM B367) is an $\alpha/\beta$ Ti alloy widely used in biomedical applications due to its corrosion resistance and high bio- and hemocompatibility [6,7]. In general, the recognized properties of Ti alloys are mainly due to the formation of a natural TiO$_2$ oxide at room temperature, which can reach a thickness of 2–10 nm [6,7]. This native thin film oxide often has a high density of defects (mainly cracks), which reduce mechanical properties such as wear resistance or chemical properties such as corrosion resistance [8]. Therefore, it becomes necessary to add thicker and more protective coatings than the TiO$_2$ natural oxide to improve the properties. Anodic oxidation is a viable technique due to its low cost, simplicity of application, and control of the coatings’ characteristics. This electrochemical process allows coatings of oxides to be obtained that have greater thickness and density than those that are naturally grown [9,10]. Among the variables of this technique that most affect the characteristics of the oxide (thickness, color, homogeneity, roughness, crystalline structure,
etc.) are current density, applied voltage, anodizing time, temperature, conductivity, and pH of the electrolyte [9–11].

Two characteristics required for coatings that will be in contact with blood are homogeneity and a low level of roughness \( (R_a \leq 50 \text{ nm}) \) to avoid the promotion of blood clots (thrombosis) [2,12]. Another property that influences the bio- and hemocompatibility of TiO\(_2\) coatings is their crystalline structure. At low pressure, TiO\(_2\) can present three crystalline phases: Anatase, rutile, or brookite. According to the literature, both amorphous phases and crystalline phases such as anatase and rutile would be bio-compatible [12].

The anodic oxidation technique—with oxidation voltages below the production of spark discharge phenomenon—can be used to obtain homogeneous TiO\(_2\) coatings with low roughness. Spark discharge produces porous and crystalline oxides and a rougher surface than desired due to the formation of sparks or electric arcs [9,13]. This phenomenon leads to a variation of the technique known as Anodic Spark Deposition [14]. The voltage at which the spark starts varies with the nature and concentration of the electrolyte employed [13,15–17]. This effect limited the oxidation voltage used in the present work, because (as previously mentioned) homogeneous and low roughness coatings are necessary for hemocompatible applications.

From the above, the primary objective of the present work was to define appropriate conditions (concentration of electrolyte and applied voltage) to obtain smooth and uniform coatings of TiO\(_2\) by anodic oxidation of Ti-6Al-4V alloy in sulfuric acid as electrolyte, to be used in the construction of a cardiovascular device.

2. Materials and Methods

2.1. Synthesis of the Coatings

2.1.1. Preparation of the Substrates

The substrates used for oxidation were flat samples of Ti-6Al-4V alloy with a surface area of \( 1 \times 2 \text{ cm}^2 \) and thickness of 0.2 cm. They were polished with abrasive SiC papers with decreasing granulometry (from \# 120 up to \# 1500), with diamond paste of 1 \( \mu \text{m} \) (Prazis, Argentina) lubricated with ethylene glycol (Cicarelli, Santa Fe, Argentina), finishing with 4:1 mix of colloidal silica (Mastermet-Buehler, Lake Bluff, IL, USA) and hydrogen peroxide. The mirror surfaces were then cleaned with water and detergent, rinsed with alcohol, and hot air dried. One of the tested substrates was not coated (TiG5).

2.1.2. Anodic Oxidation

Oxidation of the samples was carried out at room temperature (25 °C) applying a DC electric current between the Pt cathode and Ti-6Al-4V anode, separated from each other by 5 cm in a beaker glass containing the electrolyte. The electrolytes were sulphuric acid (\( \text{H}_2\text{SO}_4 \)) solutions, and the concentration was varied from 0.1 to 4 M (0.1 M, 0.5 M, 1 M, 2 M, and 4 M). The applied voltages were 20 V, 40 V, 60 V, and 70 V. Anodization time was 1 min. Immediately after oxidation, the oxidized samples were rinsed with demineralized water and dried with hot air. Evolution of voltage and current density was recorded during the oxidation. Anodization of the sample made with 4 M \( \text{H}_2\text{SO}_4 \) at 70 V had some problems due to drawbacks in cell contacts as a result of the severe anodization conditions, as evidenced by the occurrence of spark discharge and melting of the sample holder due to the high temperature achieved during spark.

The samples were labeled as follows: A letter S corresponding to the electrolyte (\( \text{H}_2\text{SO}_4 \)), followed by the concentration (in M), the letter V and the corresponding voltage (in V)—e.g., S0.1-V20, S1-V40, etc.
2.2. Coatings Characterization

The surface of the oxides was observed by optical microscopy and scanning electron microscopy (SEM), using and Arcano and Carl Zeiss Supra 40 equipment (Germany), respectively. The difference between the colors observed in the macrographs and in the micrographs is explained by the fact that in the first case it was illuminated with a white (fluorescent) light, and in the second with an incandescent light with a predominant yellow spectrum. All micrographs were taken under the same conditions of illumination, because it is extremely important to standardize the illumination to be able to compare the effects in the color, especially when the changes are very subtle.

The roughness of the coatings was measured using the Time Group (China) TR200 profilometer with a cut-off length of 0.8 mm, a sampling length of 0.8 mm, and a number of sampling of 5 in 4 mm. \(R_a\) is the average roughness and \(R_z\) is the distance between the highest peak and the lowest valley in each sampling length. Four measurements were performed on each sample, and the results were averaged, with relative error smaller than 10%.

The crystalline phases present in the coatings were analyzed by X-ray diffraction (XRD) using a Philips (Netherlands) PW 3710 diffractometer with a CuK\(\alpha\) wavelength (\(\lambda_{\text{CuK}\alpha} = 1.5418\) Å), using a Philips thin-film accessory allowing operation with a ground-beam geometry with incident angle of 1°. The crystallite size (\(L\)) of the crystalline anatase phase was estimated by Scherrer’s formula, \(L = K\lambda / (\omega\cos\theta)\), using the XRD profile. \(\lambda\) is the X-ray wavelength in nm and \(\omega\) (in radians) is the peak width of the diffraction peak profile at half maximum height. \(\theta\) is the Bragg diffraction angle of the anatase (101) peak. \(K\) is a constant related to crystallite shape, normally taken as 0.9, assuming that the crystallites are spherical.

3. Results and Discussion

3.1. Influence of the Electrolyte Concentration (H\(_2\)SO\(_4\)) on the Characteristics of the Coatings

3.1.1. Variation of Voltage and Current Density with Oxidation Time

Figure 1a shows the current density (\(i\)) and voltage (\(V\)) characteristic behaviors of a potentiostatic anodization process at low voltages [17]. When \(V\) increases, \(i\) also increases up to a maximum, indicating the formation of the TiO\(_2\) barrier layer; then, \(i\) rapidly decreases because the oxide increases its electrical resistance. When the voltage was established on 40 V, \(i\) became gradually stable due to the equilibrium between the oxide growth and dissolution rates [9,14,18]. The reduction of the oxide growth rate was probably due to titanium or oxygen diffusion through the coating becoming the controlling step. As this rate becomes small, for practical purposes, the oxide thickness reaches a limiting value, indicating that it depends on the applied voltage [17–20].

The temporal evolutions of current density in anodizations at 60 V with different electrolyte concentrations are shown in Figure 1b. The maximum and stabilization \(i\) values increased with the H\(_2\)SO\(_4\) concentration due to the increase of conductivity from 47.2 mS/cm of 0.1 M to 778.5 mS/cm of 4 M [18,21] that should induce breakdown and spark at 60 V, less than the 70 V reported for 1 M on Ti-6Al-4V anodization [13,22]. Therefore, the stabilization of \(i\) values at 2 M and 4 M curves are ten times higher than the corresponding value for 1 M.
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3.1.2. Color of the Coatings

In Figure 2, optical micrographs and macrographs (in the corner insets of each micrograph) of the samples are presented. In the macrograph, the color of the coatings obtained with different electrolyte concentration and voltage are observed. These colors are the same as observed with the naked eye.

The inset of Figure 2a shows a uniform blue color of sample S0.1-V20. When the acid concentration increased from 0.1 M to 4 M, a decrease in the tonality of this color was observed (see Figure 2a,e,i,m,q). On the other hand, the corresponding micrographs of 20 V samples show higher and clearer streaks with hue variations when the concentration increases.

Macrographs and micrographs of samples obtained at 40 V (Figure 2b,f,j,n,r) show uniform light green color and yellow color, respectively, independent of acid concentration.

Figure 1. (a) Evolution of current density and voltage during the anodic oxidation of Ti-6Al-4V at 40 V; (b) Evolution of current density during the anodic oxidation performed with different sulfuric acid concentration (1 M, 2 M, and 4 M) at 60 V.
We mentioned previously that color depends on the thickness of the coatings, but color also changed with acid concentration, probably due to different oxide growth rate given different oxide stoichiometry [15]. Another explanation for this phenomenon could be that different fractions of crystalline structures can be formed which cause changes in the density and refractive index of the oxide films [15].

In the optical micrographs of each sample, two different color tonalities are observed, homogeneously distributed on the surface. These portions with different tonalities are of a size similar to the grain size, corresponding to the microstructure of the Ti-6Al-4V substrate, so this pattern of coloration can be attributed to a different growth rate of the oxide on the different crystal
orientations of the phases of the Ti-6Al-4V substrate grains, which gives rise to oxides with slightly different thicknesses [13,23].

As observed in Figure 2, when the concentration of the H$_2$SO$_4$ increases (mainly from 1 M), the color of the coatings changed and became more intense, diminishing the difference between colors in the previously described pattern. This could be because the increase in concentration and conductivity of the electrolyte diminishes the differences in the growth rate of the oxides on the different phases or crystal orientations of the phases of the substrate.

Despite the small differences observed in the colors obtained using different concentrations of the electrolyte, the oxide colors can be used to make a quick qualitative identification of the thickness, from an established scale for each electrolyte. With 1 M H$_2$SO$_4$ in pre-spark conditions, a relationship between color, voltage, and thickness (2.4 nm/V) was previously established [13,24].

### 3.1.3. Morphology of the Coatings

Figure 3 shows SEM images of anodized samples with different voltages and concentration of electrolyte. Anodized samples at 20 V (not shown) and 40 V (Figure 3a,d,g,j) showed different surface morphologies but none of them presented porous surfaces. In SEM images of samples anodized at 60 V (Figure 3b,e,h,k), different isolated pore structures are observed. In S0.1-V70 and S0.5-V70 samples, irregular surfaces are observed, and in S1-V70 and S2-V70 samples, pores are larger and agglomerated.
As previously mentioned, many factors influence the morphology; Masahashi et al. [25] found that both roughness and surface area increase with the concentration of sulfuric acid. On the other hand, Kim and Ramaswamy [26] observed the appearance of microcracks in the oxides with the increase of the electrolyte concentration. However, in the present research, the most significant changes in morphology were observed with the increase of the voltage with each concentration of H₂SO₄ used, but not with the increase of the concentration independent of the voltage.

With respect to roughness, coatings have values of average roughness (Rₐ) in the range of 6 nm and 32 nm (Table 1), reproducing the surface roughness of the polished substrate (20 nm) and not changing appreciably with the concentration of H₂SO₄. That range of values complies with the desired values for the application of the manufacture of cardiovascular devices (Rₐ ≤ 50 nm) [2,11]. The lower roughness values (Rₐ and Rₛ) were obtained for samples anodized at 20 V and 40 V. However, the increase of the roughness and porosity with the oxidation voltage was observed mainly in the values of Rₛ in the samples obtained at 60 V and 70 V with the solutions of H₂SO₄ of concentrations of 0.5 M, 1 M, and 2 M (Table 1). As the presence of porosity in samples made with voltages up to 60 V could promote clot formation, voltages lower than 60 V have to be used to obtain homogeneous and low roughness coating suitable for hemocompatibility.

**Table 1. Roughness (Rₐ and Rₛ) and crystalline phases of the coatings.**

<table>
<thead>
<tr>
<th>Samples</th>
<th>Rₐ (nm)</th>
<th>Rₛ (nm)</th>
<th>Crystalline Phase</th>
</tr>
</thead>
<tbody>
<tr>
<td>TiG5</td>
<td>20</td>
<td>100</td>
<td>α and β</td>
</tr>
<tr>
<td>S0.1-V20</td>
<td>7</td>
<td>54</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.1-V40</td>
<td>9</td>
<td>82</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.1-V60</td>
<td>12</td>
<td>98</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.1-V70</td>
<td>11</td>
<td>80</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.5-V20</td>
<td>10</td>
<td>90</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.5-V40</td>
<td>8</td>
<td>73</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.5-V60</td>
<td>18</td>
<td>121</td>
<td>amorphous</td>
</tr>
<tr>
<td>S0.5-V70</td>
<td>14</td>
<td>123</td>
<td>amorphous</td>
</tr>
<tr>
<td>S1-V20</td>
<td>19</td>
<td>31</td>
<td>amorphous</td>
</tr>
<tr>
<td>S1-V40</td>
<td>6</td>
<td>61</td>
<td>amorphous</td>
</tr>
<tr>
<td>S1-V60</td>
<td>13</td>
<td>132</td>
<td>amorphous</td>
</tr>
<tr>
<td>S1-V70</td>
<td>32</td>
<td>307</td>
<td>anatase (21 nm) *</td>
</tr>
<tr>
<td>S2-V20</td>
<td>15</td>
<td>95</td>
<td>amorphous</td>
</tr>
<tr>
<td>S2-V40</td>
<td>12</td>
<td>90</td>
<td>amorphous</td>
</tr>
<tr>
<td>S2-V60</td>
<td>16</td>
<td>151</td>
<td>amorphous</td>
</tr>
<tr>
<td>S2-V70</td>
<td>19</td>
<td>151</td>
<td>anatase (7 nm) *</td>
</tr>
<tr>
<td>S4-V20</td>
<td>13</td>
<td>93</td>
<td>amorphous</td>
</tr>
<tr>
<td>S4-V40</td>
<td>15</td>
<td>100</td>
<td>amorphous</td>
</tr>
<tr>
<td>S4-V60</td>
<td>14</td>
<td>111</td>
<td>anatase (15 nm) *</td>
</tr>
</tbody>
</table>

* Crystallite size of anatase phase is indicated in brackets.

Figure 3. SEM micrographs of anodic oxidized samples.
3.1.4. Structure of the Coatings

The diffractograms of the samples obtained under glancing incidence of 1° are shown in Figure 4, grouped by voltages. In Figure 4a, it can be seen that the diffractograms of the samples obtained at 40 V do not show any anatase or rutile peak. Only the corresponding peaks of the alpha (α) and beta (β) phases of Ti-6Al-4V alloy were observed. The absences of the peaks of crystalline oxide phases may be due to the coatings being completely amorphous or to crystallite sizes being too small to be detected by XRD. The diffractograms of samples obtained at 60 V are shown in Figure 4b, where in the spectra of S4-V60 sample, anatase peak (101) at 2θ 25.29° is observed. This peak is clearer in the inset, where it is also observed that the anatase peak is not present in the S2-V60 sample. In Figure 4c, diffractograms of samples obtained at 70 V are shown, where the anatase peak appeared in samples obtained with 1 M and 2 M H2SO4 (S1-V70 and S2-V70).

![Figure 4a](image1)

![Figure 4b](image2)
Briefly, with 0.1 M and 0.5 M H$_2$SO$_4$, no crystalline coatings over the entire range of analyzed voltages (20–70 V) were obtained. With 1 M and 2 M H$_2$SO$_4$, crystalline coatings from 70 V were obtained; with 4 M, anatase appeared from 60 V. These results indicate that with an increase in the concentration of sulfuric acid, the voltage at which the transformation of the amorphous coatings to anatase occurs decreases, due to the increase of the conductivity with the concentration, which could favor the crystallization at lower voltage.

Thermal treatments will be necessary to crystallize amorphous coatings obtaining up to 60 V for 4 M H$_2$SO$_4$ and 70 V for lower H$_2$SO$_4$ concentrations [27].

Regarding the size of the anatase crystallites in the crystalline coatings (Table 1), it is known that anatase is a metastable phase whose thermodynamic stability is dependent on the size of the crystallite; the anatase is more stable than rutile when its crystallites are smaller than a critical size, which in this case seems to be larger than 21 nm [28,29].

4. Conclusions

The study of the anodic oxidation of Ti-6Al-4V alloy in sulfuric acid in different concentrations as electrolyte at constant voltages of 20 V to 70 V yielded the following conclusions:

Different interference colors of the coatings were obtained according to the applied voltage and the electrolyte used. Despite the differences observed in the colors obtained using different concentrations of the electrolyte, for all cases, the color of the oxides became more intense and tonality differences diminished with the increase of the concentration of H$_2$SO$_4$, especially from 1 M. Additionally, tonality differences diminished at 40 V and 60 V.

With respect to morphology, with all concentrations, porosity was observed in samples surfaces at 60 V, limiting the usable voltage. The lower roughness values ($R_a$ and $R_z$) were obtained for samples anodizing at 20 V and 40 V.

Regarding the crystalline structure of the oxides, up to 60 V the coating was amorphous, and then starting at 70 V, it began to crystallize to the anatase phase in coatings obtained with 1 M and 2 M H$_2$SO$_4$. An increase in the concentration of H$_2$SO$_4$ decreased the voltage at which the transformation of amorphous to crystalline coatings occurred, and with 4 M H$_2$SO$_4$, the anatase phase appeared at 60 V.

To obtain non-porous, homogeneous, and low roughness coatings to avoid the promotion of blood clots, the voltage to work with is 40 V at a concentration of 1 M sulphuric acid. Those

Figure 4. XRD patterns of the substrate and oxidized samples with different electrolytes at different voltages: (a) 40 V; (b) 60 V; (c) 70 V. $\alpha = \text{anatase, } \alpha = \alpha \text{ phase of TiG5, and } \beta = \beta \text{ phase of TiG5.}$
anodizing conditions produce coatings with the most appropriate characteristics for the manufacture of cardiovascular devices.

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